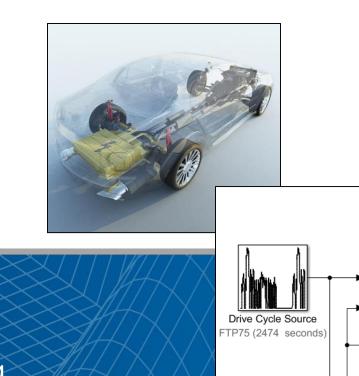
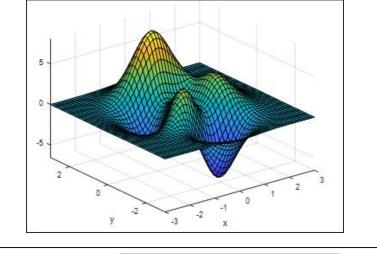


# **Objective Drivability Calibration**

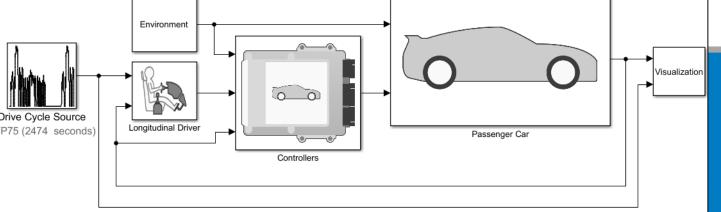
MathWorks Automotive Conference

April 30<sup>th</sup>, 2019





Co-Authors: Jason Rodgers\* & Jan Janse van Rensburg



MathWorks



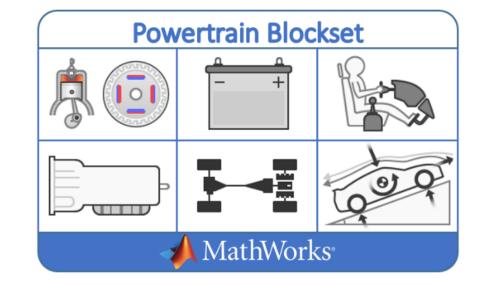
### Presenter

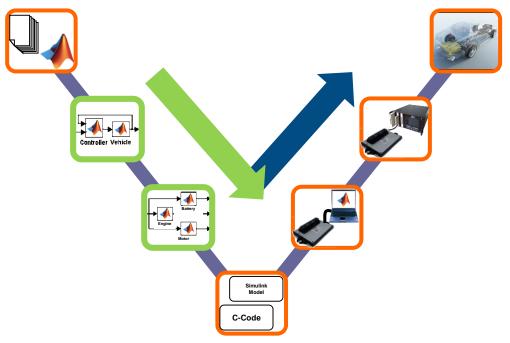
- Jason Rodgers
  - MathWorks Senior Application Engineer
    - Vehicle Dynamics Blockset
    - Powertrain Blockset
    - Model Based Calibration Toolbox
  - Previous experience at Toyota R&D
    - System Optimization and Control engineer
    - Optimizing powertrain design and controls subject to various constraints (cost, FE, drivability, etc.)
  - Education
    - BSME and MSME, University of Michigan
  - Areas of interest
    - Enabling Model-Based Design using physical modeling
    - Applying optimization techniques to modeling and control problems
    - Applying new technologies such as Deep Learning to Automotive problems



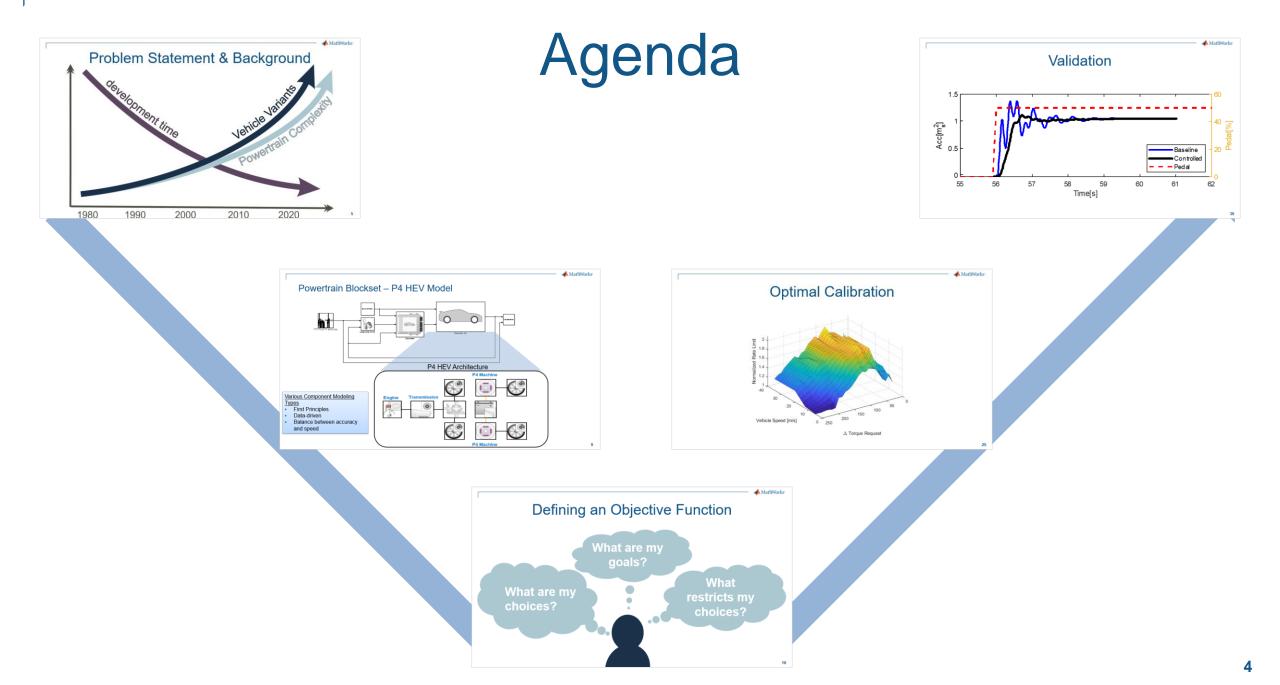
# Key Takeaways

- Powertrain Blockset is capable of simulating low frequency drivability behavior
- Model re-use from early planning phase can be used to jumpstart calibration efforts
- Objective-based calibration can:
  - Improve calibration time
  - Account for performance trade-offs
  - Trace back to requirements
  - Objective and not subjective  $\rightarrow$  repeatable

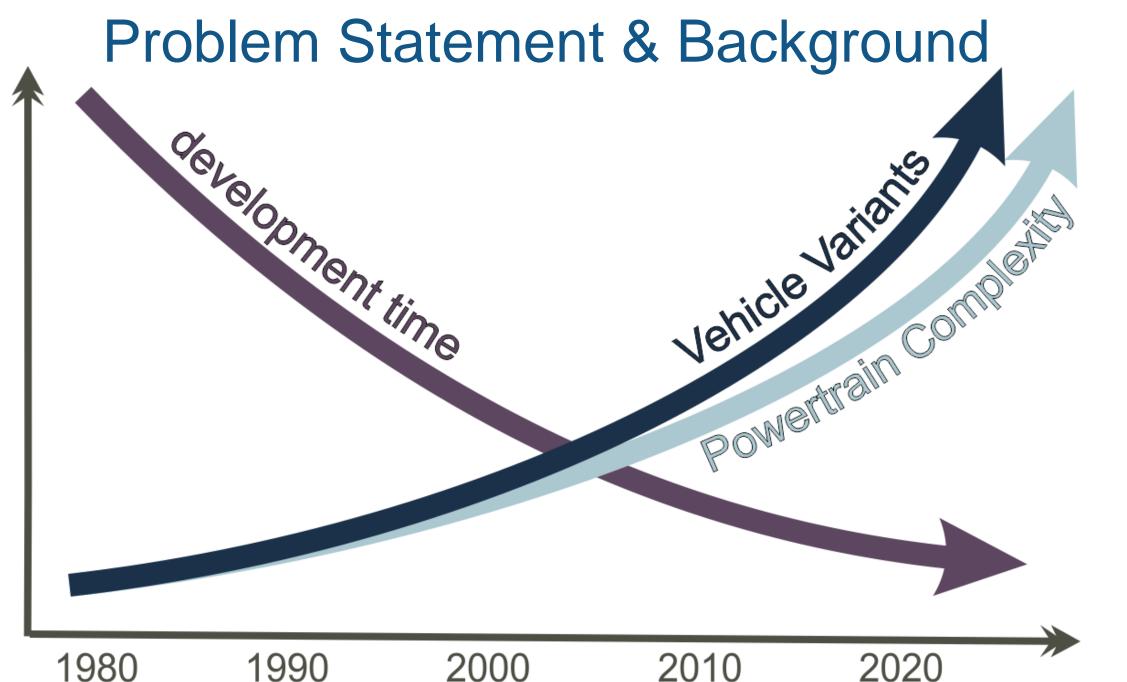








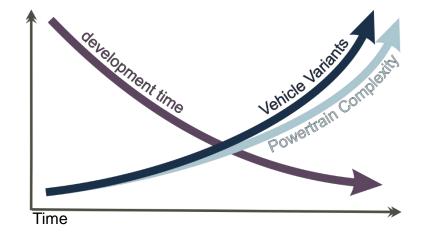


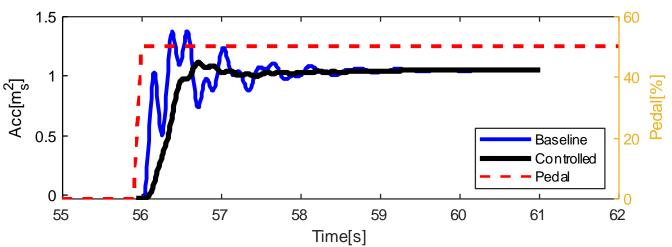




### **Problem Statement**

- What is the problem?
  - ECU can have dramatic effect on drivability
  - Manual calibration is time sink
  - Ratings are defined by experienced but subjective drivers
  - Efficiency improvements are needed
    - Decreasing development time
    - Increasing powertrain complexity and number of variants
- How to solve the problem?
  - Use objective based approach to tune ECU calibration parameters
    - I. Requirements driven
    - II. Objective based Repeatable
    - III. Automated Time savings
    - IV. Optimal with respect to requirements







# Background

### What is drivability?

 Response characteristic of the vehicle to driver inputs under different driving conditions

- Want the driver to be as comfortable as possible
  - Hesitation
  - Sluggish
  - Hard start
  - Noise/Oscillations

- Drivability is affected by many sources
  - Gear shifts
  - Engine Idle
  - Braking
  - Acceleration
  - Etc.

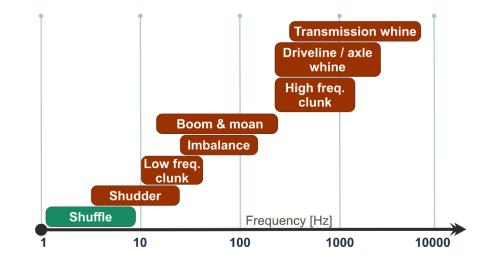


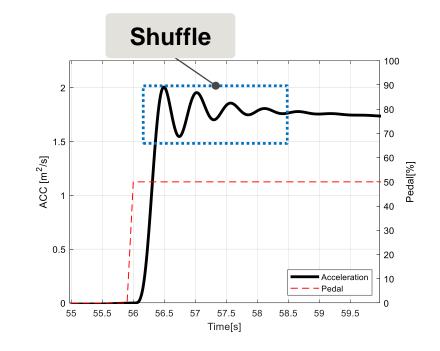


### Background

### What are we focusing on?

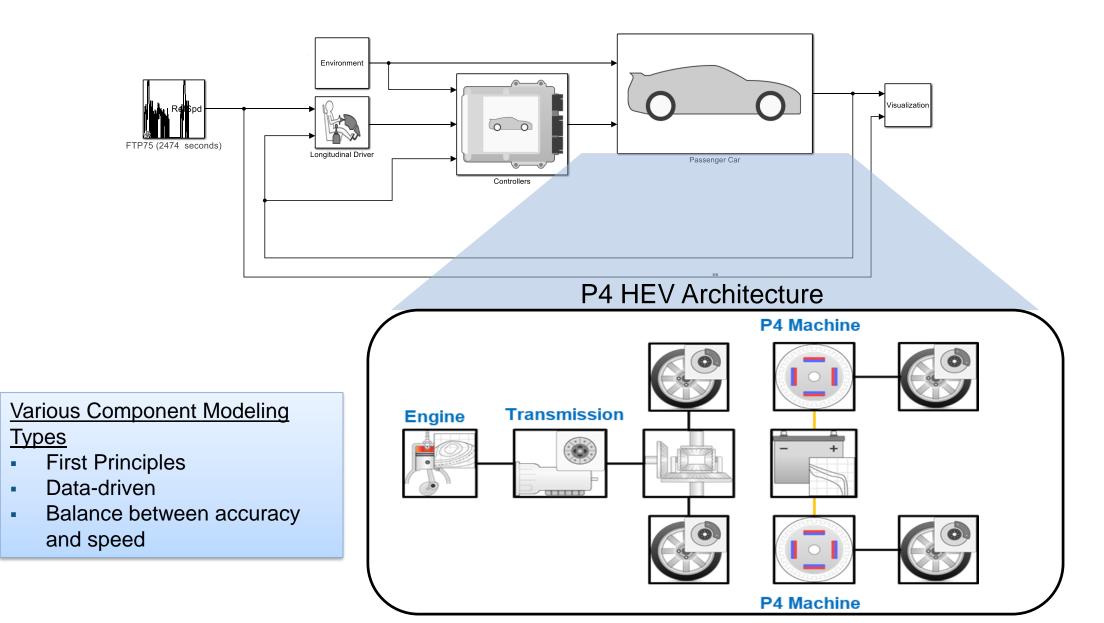
- Shuffle related to tip in
  - NVH longitudinal effect caused by sudden changes in the drive torque
  - Some room to optimize hardware but controller is more cost effective
  - 2-8 Hz depending on the gear
- Not considering shift shock, clunk, or higher order modes
- Acceleration is measured at CG
- No gear shift during tip in event







### Powertrain Blockset – P4 HEV Model





## Powertrain Blockset – P4 HEV Model

- P4 HEV Powertrain model
  - Started from reference application and modified for \_ testing and added tip-in controller

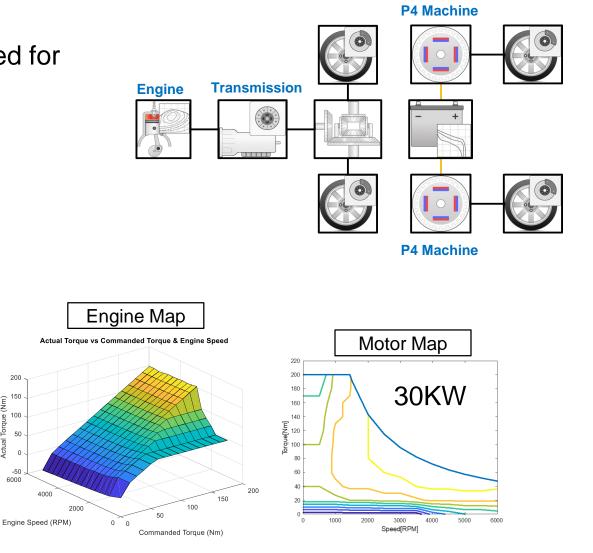
(MM) <u>
</u>
100
·

50

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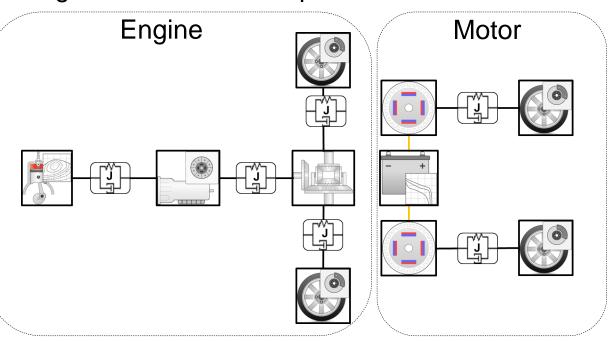
- Model fidelity is typical for Fuel Economy and acceleration studies
- Model reuse
- Engine
  - 1.5L L4 95kW(126hp) @5500RPM
  - Map-Based Model \_
- 2 P4 30kW Motors
  - Map-Based Model
- 1.3 kWh Battery
  - Map-Based Model





## P4 Component Modeling

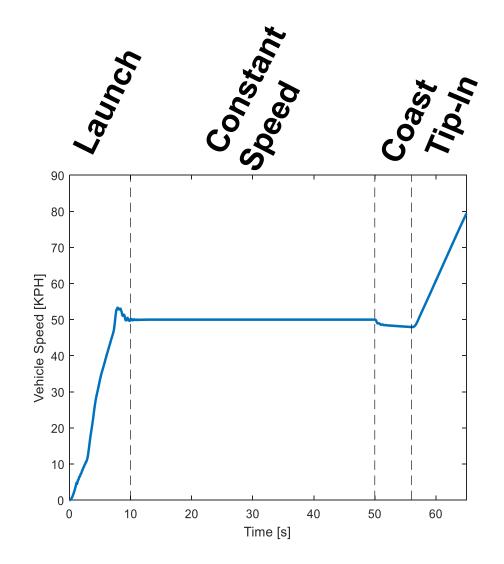
- Driveline oscillations are captured by rotational inertia and compliance blocks that exist in reference model
- Linear damping and stiffness
  - Openness of model allows for replacing with nonlinear components
- 2 Torque Paths
  - Engine
  - Motor





# **Driving Scenario**

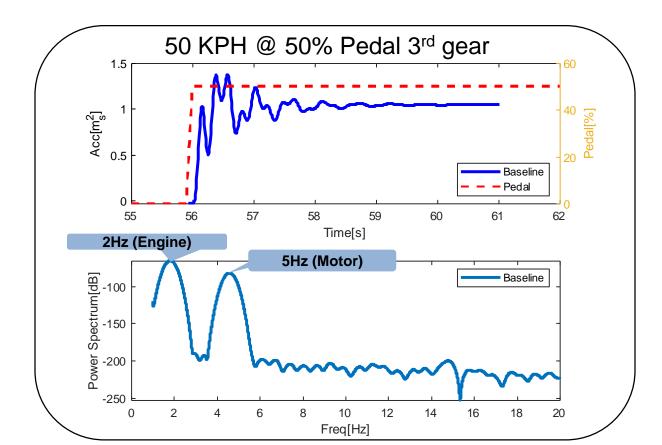
- What scenario are we using?
  - 1. Accelerate to Constant Speed
  - 2. Hold Speed and shift to desired gear. Allow transients to subside.
  - 3. Let off pedal
  - 4. Apply pedal step input





### **Tip-In Acceleration Response**

- Initial response has large amounts of shuffle oscillations
  - Model is able to capture the first mode (shuffle) for both torque paths
  - Response attenuation is required to improve drivability





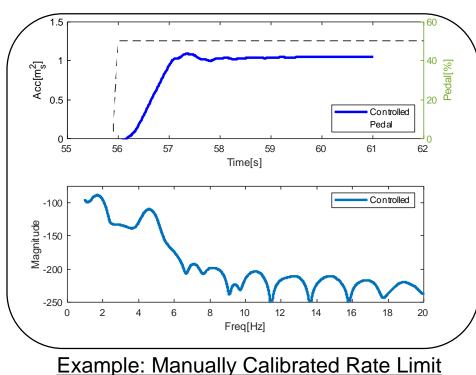
# Tip-In Acceleration Response

- How to improve?
  - Spark Control (on engine side only)
  - Fixed Rate-Limit on torque request or pedal input
  - Scheduled Rate-Limit
  - Optimal Control e.g. Model Predictive Control

### First Pass at Improvements:

- Reduced oscillations but response is slow
- Is a function of gear, speed, and torque request  $\rightarrow$  scheduled rate-limit
- Long manual process to do by hand (weeks)
- How to balance responsiveness and oscillations?

### **Define an Objective Function and Optimize!**





# Defining an Objective Function



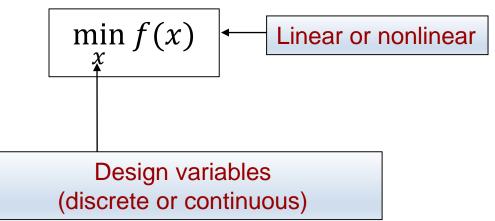


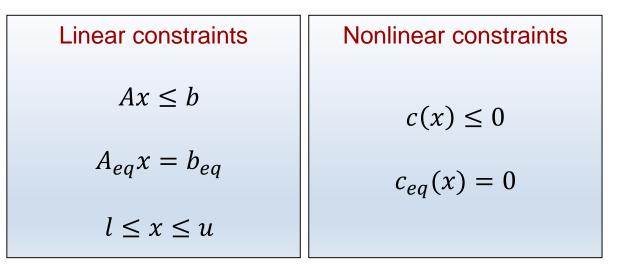
# **Optimization Introduction**

- Objective function What you are trying to achieve?
  - Minimize measured signal
- Design variables What parameters need to be adjusted?
  - Physical model parameters
  - Controller gains
- Constraints What are the bounds or constraints of the design variables?
  - Min/Max values
  - Can handle inside objective function

# *Minimizing* (or maximizing) objective function(s) subject to a set of constraints

### **Objective Function**







# Formulating an Optimization Problem for Objective Drivability



What are my goals?

- Minimize oscillations
- Minimize response time

#### Variables

#### What are my choices?

#### • Rate limit

- Gear
- ATorque Request
- Vehicle speed

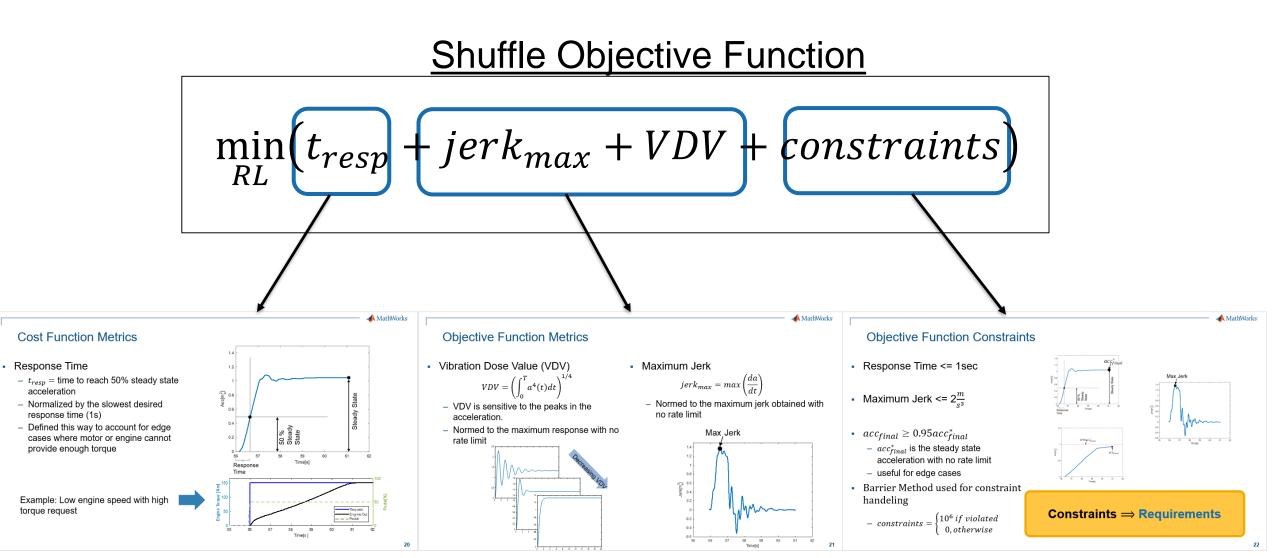
#### Constraints

What restricts my choices?

- Response Time
- Jerk
- Etc.



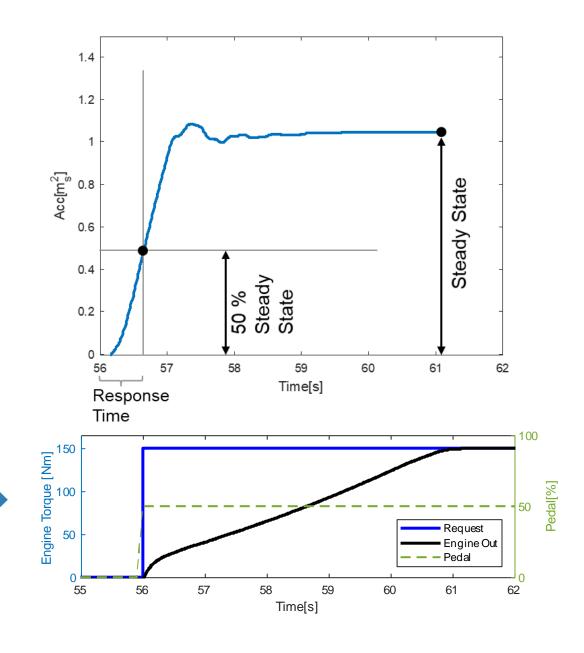
### **Objective Function**





## **Cost Function Metrics**

- Response Time
  - $t_{resp}$  = time to reach 50% steady state acceleration
  - Normalized by the slowest desired response time (1s)
  - Defined this way to account for edge cases where motor or engine cannot provide enough torque

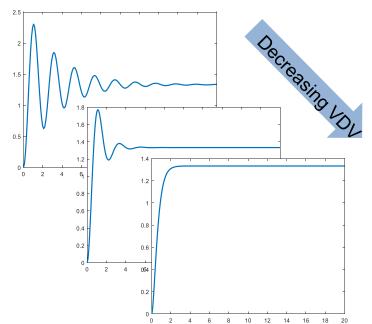


Example: Low engine speed with high torque request



### **Objective Function Metrics**

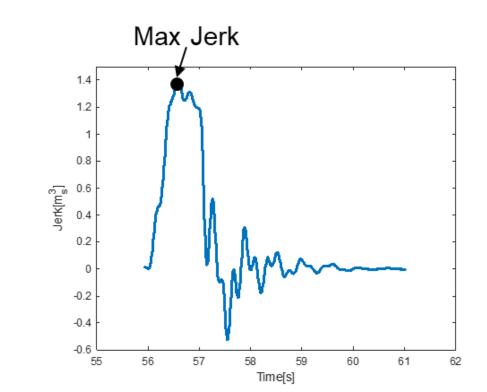
- Vibration Dose Value (VDV)  $VDV = \left(\int_0^T a^4(t)dt\right)^{1/4}$ 
  - VDV is sensitive to the peaks in the acceleration.
  - Normed to the maximum response with no rate limit



Maximum Jerk

$$jerk_{max} = max\left(\frac{da}{dt}\right)$$

 Normed to the maximum jerk obtained with no rate limit

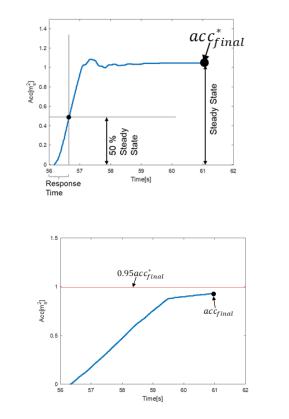


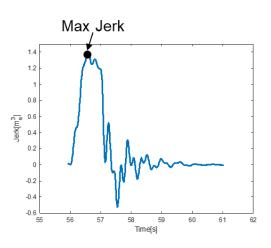


# **Objective Function Constraints**

- Response Time <= 1sec</li>
- Maximum Jerk  $\leq 2\frac{m}{s^3}$
- $acc_{final} \ge 0.95acc^*_{final}$ 
  - $acc_{final}^{*}$  is the steady state acceleration with no rate limit
  - useful for edge cases
- Barrier Method used for constraint handeling

$$- \ constraints = \begin{cases} 10^6 \ if \ violated \\ 0, otherwise \end{cases}$$





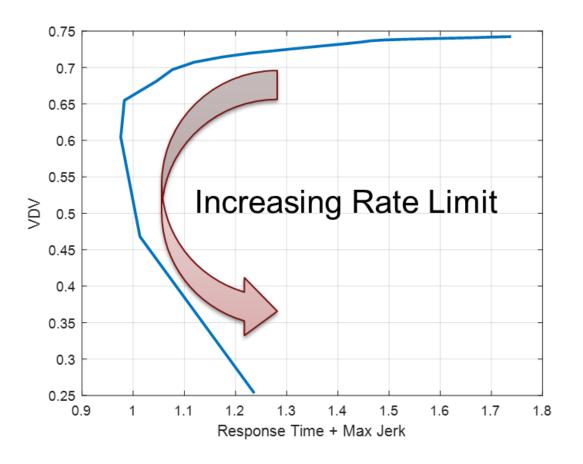
# **Constraints** ⇒ **Requirements**



# **Objective Function**

### **Observations**

- Pareto curve exists between oscillations and response time
  - the faster the response, the more oscillations

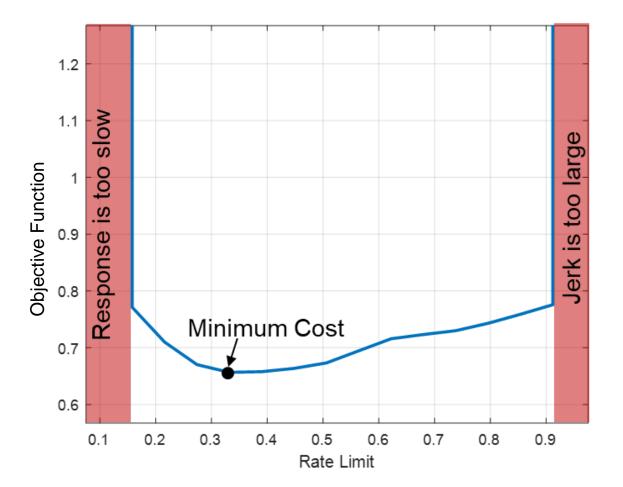




## **Objective Function**

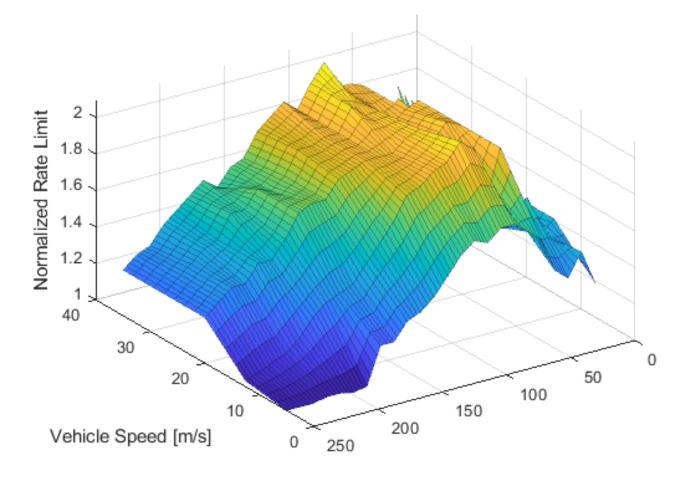
### **Observations**

- Objective function:
  - Can be non-smooth
  - Can have multiple minima





# **Optimal Calibration**

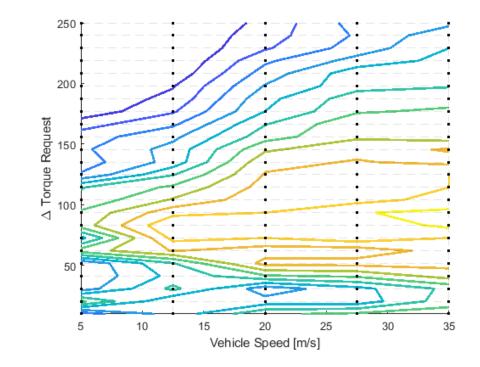


 $\Delta$  Torque Request



# **Calibration Process**

- Intel Xeon E5 processor 3.6GHz, 6 cores
- 64GB RAM
- 1806 Optimal Rate-Limits
  - 7 total maps (6 for engine, 1 for motor)
  - 24 Atorque breakpoints
  - 5 speed breakpoints
- Traditionally, this process could take days or weeks for manual calibration
- 10 hours to automatically calibrate using pattern search global optimization algorithm

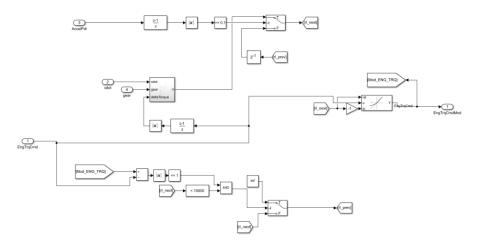




📣 MathWorks<sup>®</sup>

# **Tip-In Controller**

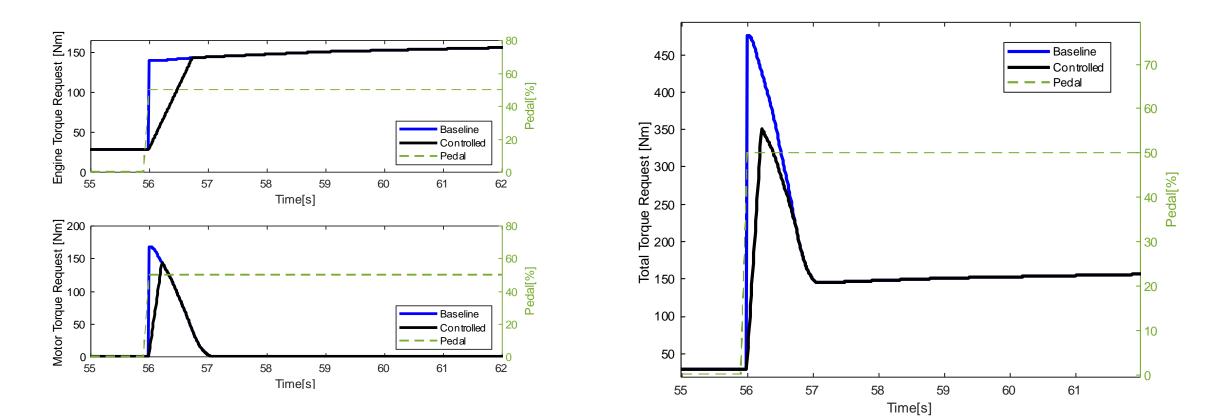
- Rate limit is calculated as a function of |ΔTorque request|, vehicle speed, and Gear (engine side only)
- Rate limit is applied when judged a tip in response
  - |∆Torque request| >10Nm
  - Vehicle Speed > 2 MPH
- Rate limit held until modified torque is near final desired torque value.





## **Tip-In Controller**

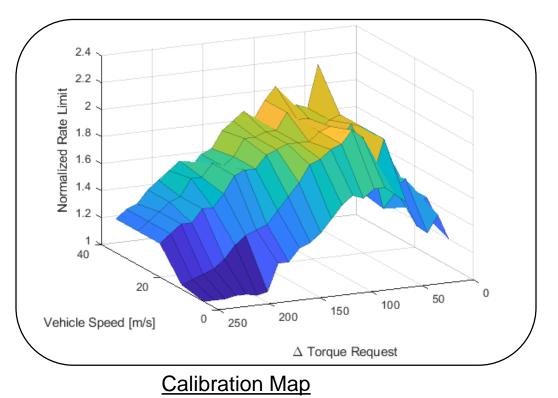
Controlled Response

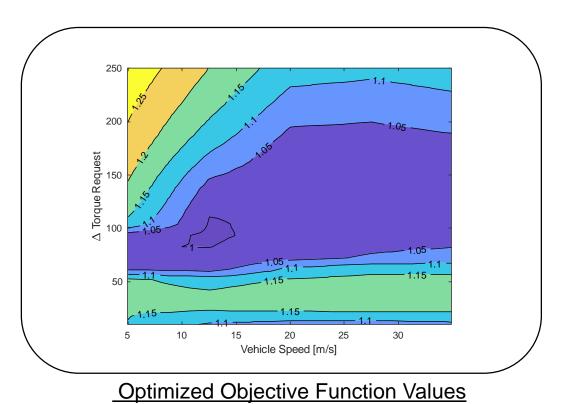




### **Calibration Tables**

- Areas of high sensitivity in the objective function can be used to redefine map breakpoints
- Example results for 5<sup>th</sup> gear

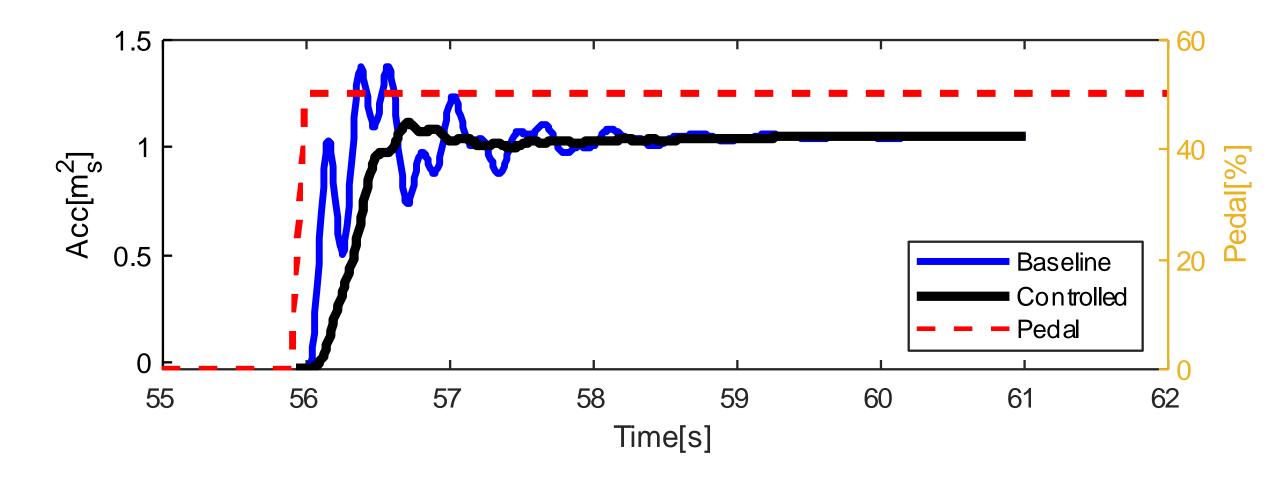




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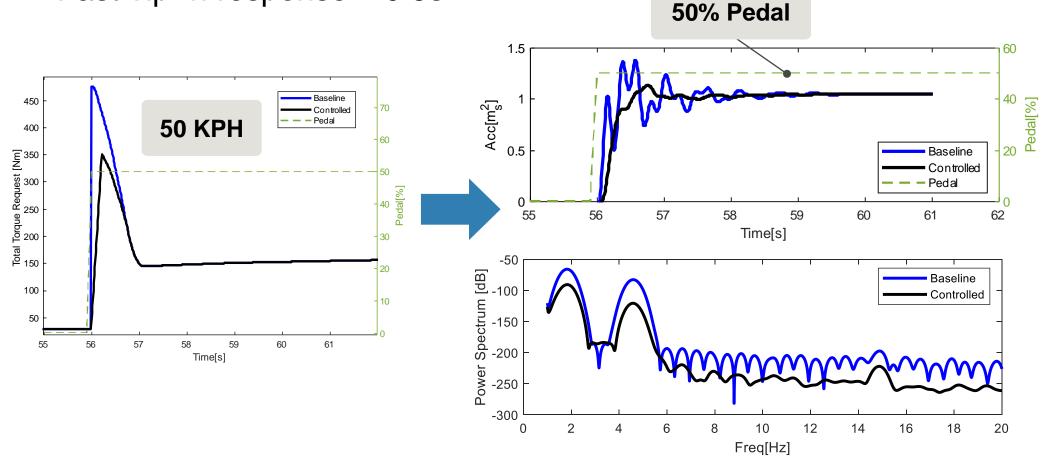
# Validation





## **Tip-In Results**

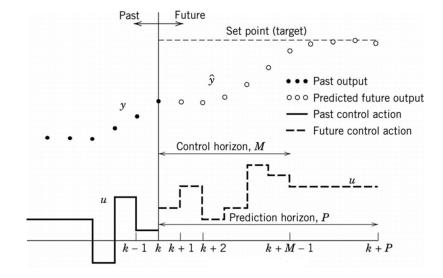
- First engine and motor modes have decreased greatly (~50dB)
- Fast Tip-In response 0.5s



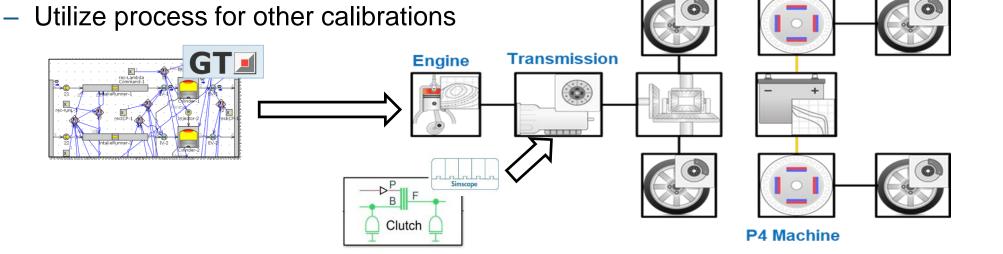


## **Next Steps**

- What are possible next steps?
  - Investigate more control options
    - Use sensitivity analysis to refine breakpoints in calibrated maps
    - Model Predictive Control with consideration for Fuel Economy
  - Process can be reused as model fidelity increases
    - GT Engine model
    - Simscape Driveline



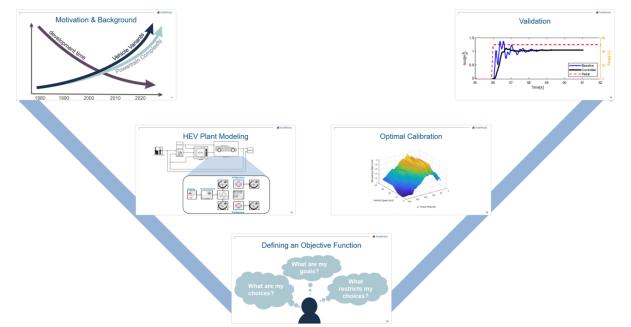
**P4 Machine** 





## Summary

- A process for using an objective function to automate and improve shuffle response was shown
- Virtual calibration allowed process to be done in hours instead of weeks
- Along with FE and Acceleration characteristics, can also start to consider some drivability metrics during early phase planning





# Thank You



Jason Rodgers, MS Senior Application Engineer jrodgers@mathworks.com





### References

Wellmann, T., Govindswamy, K., Braun, E., and Wolff, K., "Aspects of Driveline Integration for Optimized Vehicle NVH Characteristics," SAE Technical Paper 2007-01-2246, 2007

Atabay, O., Ötkür, M., & M Ereke, İ. (2018). Model based predictive engine torque control for improved drivability. *Proceedings of the Institution of Mechanical Engineers, Part D: Journal of Automobile Engineering*, 232(12), 1654–1666. <u>https://doi.org/10.1177/0954407017733867</u>

Jauch, C.; Tamilarasan, S.; Bovee, K.; Guvenc, L.; Rizzoni, G. Modeling for drivability and drivability improving control of HEV. Control Eng. Pract. 2018, 70, 50–62. [CrossRef]

Wei,X.,&Rizzoni,G.(2004).Objective metrics of fuel economy, performance and driveability–A review.SAETechnicalPaper,2004(2004-01-1338), http://dx.doi. org/10.4271/2004-01-1338.